Simulated Wave Generation—WGEN

The program WGEN (Simulated Wave Generation) is a subroutine subprogram that creates an acceleration time history for simulated earthquake motions consistent with the target Ohsaki's spectrum (5% damping factor) when the magnitude and epicentral distance of an earthquake are given.

WGEN (Simulated Wave Generation)

[Purpose]

When the magnitude and epicentral distance of an earthquake are given, to generate an acceleration time history consistent with Ohsaki's velocity response spectrum of a 5% damping factor.

[Usage]

(1) How to connect

CALL WGEN (EM, R, NN, IR, ACC, ND, DT, AMAX, VMAX, MYCYCL, ERR, UW1, UW2)

Argument	Туре	Parameter in calling program	Return Parameter
EM	R	Magnitude of earthquake	Unchanged
R	R	Epicentral distance (unit : km)	Unchanged
NN	Ι	Number of Acceleration data	Unchanged
IR	Ι	Any integer to initiate sequence for random number generation	Changed
ACC	R 1-D array (ND)	No need to input here	Simulated acceleration time history (unit: Gal)
ND	Ι	Dimension size of ACC, VW1 and VW2 in calling program (ND .GE. NN)	Unchanged
DT	R	No need to input here	Time interval of acceleration time history (unit: sec)
AMAX	R	No need to input here	Max. acceleration of time history (unit: Gal)

VMAX	R	No need to input here	Max. velocity of time history (unit: cm/sec)
MYCYCL	Ι	Max. number of iteration	Actual number of iteration
ERR	R	Root-mean-square allowable error for convergence	Actual error
UW1	R 1-D array (ND)	No need to input here	(Workspace)
UW2	R 1-D array (ND)	No need to input here	(Workspace)

(2) Necessary subroutines and function subprograms ENVL, OHSP, VELK, FAST, CRAC, IACC, ERES, RAND

(3) Remarks

NN must be a power of 2 not exceeding 4096.

[Calculation Method]

The structure of the program is approximately as follows.

(a) Arguments

NN is the number of data in the simulated seismic motion time history to be generated, and should not exceed 4096. The following *NN* may be appropriate depending on the magnitude of the earthquake. If you want a *NN* that is not a power of 2, you can make it a power of 2 by adding some trailing zeros.

Magnitude M	6	7	8
NN	512	1024	2048
Duration T_d (sec)	12.2	24.9	50.8
Time Interval Δt (sec)	0.024	0.024	0.025

The argument IR is an initial value given in the form of **RAND**(IR) to invoke the function subprogram for generating uniformly distributed random numbers between 0 and 1 that the user selects from his library and quotes in the program (here, the name is tentatively given as **RAND**). The argument IR is depending on the system that provide **RAND**(IR). Depending on the initial value of the argument IR, different seismic motions can be generated for the same given conditions.

The argument *ERR* is the allowable error to terminate the iterative calculation, and from a practical standpoint, it does not need to be smaller than 5%. In the case of *ERR*=0.05, the calculation converges after about 4 to 6 iterations, so in the usual case, it is sufficient to set the argument *MXCYCL*, which gives the maximum number of iterations, to around 10.

(b) Phase differences

Call the subroutine **ENVL** to find the duration T_d and calculate the time interval Δt of the time history. The envelope curve E(x) is defined by 33 points, including the points corresponding to its two ends, i.e., time 0 and T_d (x=0 and x=1), or in other words, the points that divide the x-axis between 0 and 1 into 32 equal parts. Next, find the cumulative probability density distribution EE(x) by sequentially adding the values of the envelope curve E(x) starting from 0, and then find the value of x such that EE(x) = p when p is an arbitrary random number uniformly distributed between 0 and 1.

If we repeat this for (NN/2-2) random numbers, we get a sample of (NN/2-2) x values distributed between 0 and 1. Converting these to a distribution between 0 and (-2π) , a set of phase differences *PDI*F, i.e., $\Delta \phi_k$ ($k = 1, 2, \dots, NN/2 - 2$), can be determined. The shape of the distribution of these phase differences will be similar to the shape of the envelope curve. Therefore, we can expect that the simulated earthquake motion produced will have the envelope shape given by the subroutine *ENVL* to a good approximation.

(c) Phase angles

Once the phase differences are determined, the phase angle *PHI* can be calculated in the following order, assuming that *PHI* (1) can be ignored and *PHI* (2) is assumed to be $\phi_2 = 0$.

$$\phi_{k+1} = \phi_k + \Delta \phi_k$$
 $k = 2, 3, \dots, NN/2 - 2$

(d) Target spectrum and Fourier first order approximation

In this section, we first calculate the vibration period of each component.

$$T_k = T_d / k$$
 $k = 2, 3, \cdots, NFOLD$

 T_1 is infinity, but the program assumes that $T_1 = 2T_2$.

Since the Ohsaki's spectrum, which is the target spectrum, is originally defined with a period between 0.02 and 2 sec, we find the minimum order *KMIN*, the maximum order *KMAX*, and the number of periods *NE* that fall within this range.

Next, call the subroutine **OHSP** to obtain the velocity response spectrum with a damping factor of 0% at each period point T_k (set to 0 outside the above range), $(S_V)_k^{h=0}$, and use the approximate equality of this spectrum and the Fourier amplitude spectrum as a first approximation of the amplitude F_k . Call the **OHSP** again to obtain the velocity response spectrum with a damping factor of 5%, $(S_V)_k^{target}$, which will be the target spectrum in the future.

(e) Iterative approximation

The first iteration (*NCYCL*=1) is started, and the complex Fourier coefficients C_k are obtained from the first approximation of F_k and the phase angle ϕ_k . The inverse Fourier transform of C_k is then used as the first approximation of the acceleration time history *ACC*.

(f) Base-line correction

At this point, it is desirable to call the subroutine **CRAC** to perform a baseline correction of the acceleration time history. The corrected time history is then Fourier transformed to obtain a new first approximation of the amplitude F_k .

(g) Correction of Fourier amplitude

For the baseline-corrected acceleration time history of the first approximation, we call the subroutine **ERES** to obtain the velocity response spectrum $(S_V)_k$ with a damping factor of 5%, which does not match the target spectrum $(S_V)_k^{target}$. So, we calculate the ratio of the two as follows,

$$r(k) = (S_V)_k^{target} / (S_V)_k$$

Modify the amplitude F_k as $F_k \rightarrow r(k) \cdot F_k$ and use this as the second approximation of F_k to enter the second iteration (*NCYCL* = 2).

(h) Convergence error

The same calculation is repeated below, and the calculation is terminated when the number of iterations reaches a predetermined value (*MXCYCL*), or when the average of the squares of the error ratio r(k) becomes smaller than the allowable error *ERR*. At this point, the data stored in the array *ACC* is the acceleration time history of the simulated earthquake motion to be evaluated.

The arithmetic of the program has been described above, but we would like to add a few more things related to this program.

i) Depending on the numerical value of the argument *IR*, different seismic motions can be generated for the same magnitude and the same epicentral distance of the earthquake. By using this program, the maximum acceleration and velocity of the generated earthquake motion would not be very far from the maximum acceleration and velocity calculated by **OHAC** and **VELK**, respectively, regardless of the value of *IR*. However, if possible, it is desirable that they are very close. Although it is difficult to evaluate objectively, one of the requirements for simulated earthquake ground motions is that, if possible, the shape of the generated ground motion should have the characteristics of natural ground motions.

In practice, we will repeat several trials, giving appropriate values to the argument *IR*, and try to find one that meets these conditions. You will probably be able to reach a satisfactory result within 10 trials.

ii) As described previously in section (d), the arithmetic method of this program first determines the velocity response spectrum $(S_V)_k^{h=0}$ with 0% damping factor at each period point T_k . Then, focusing on the approximation between this velocity response spectrum and the Fourier amplitude spectrum, the first approximation of the Fourier amplitude F_k is determined. Then, in subsequent iterations, successive approximations of F are calculated using the velocity response spectrum $(S_V)_k^{target}$ with a damping factor of 5% as the target spectrum.

However, if we omit the step of finding $(S_V)_k^{h=0}$ for the sole purpose of determining the first approximation of F_k , and instead use $(S_V)_k^{target}$ with a damping factor of 5% as the first approximation of F_k from the beginning, the result will be almost the same.

[Program List]

С	* * * * * * * * * * * * * * * * * * * *	WGEN	1
С	SUBROUTINE FOR SIMULATED WAVE GENERATION	WGEN	2
С	* * * * * * * * * * * * * * * * * * * *	WGEN	3
С		WGEN	4
С	CODED BY Y. OHSAKI	WGEN	5
С		WGEN	6
С	PURPOSE	WGEN	7
С	TO GENERATE, FOR GIVEN MAGNITUDE AND EPICENTRAL DISTANCE OF	WGEN	8
С	AN EARTHQUAKE, AN ACCELERATION TIME-HISTORY CONSISTENT WITH	WGEN	9
С	OHSAKI'S VELOCITY RESPONSE SPECTRUM OF 5-PERCENT DAMPING	WGEN	10
С		WGEN	11

С	USAGE	WGEN	12
С	CALL WGEN (EM, R, NN, IR, ACC, ND, DT, AMAX, VMAX, MXCYCL, ERR, UW1, UW2)	WGEN	13
С		WGEN	14
С	DESCRIPTION OF ARGUMENTS	WGEN	15
С	EM - MAGNITUDE OF EARTHQUAKE	WGEN	16
С	R – EPICENTRAL DISTANCE IN KILOMETERS	WGEN	17
С	NN – TOTAL NUMBER OF DATA IN TIME-HISTORY	WGEN	18
C	IR – ANY INTEGER TO INITIATE THE SEQUENCE FOR RANDOM	WGEN	19
С	NUMBER GENERATION	WGEN	20
С	ACC(ND) = ACCELERATION TIME-HISTORY IN GALS	WGEN	21
C	ND $-$ DIMENSION OF ACC 11W1 11W2 IN CALLUNG PROGRAM	WGEN	21
C	DT – TIME INTERVAL IN TIME-HISTORY IN SEC	WGEN	22
C	AMAY - MAY ACCELERATION OF TIME-HISTORY IN CALS	WCEN	$\frac{20}{24}$
C	WAX - MAX VELOCITY OF TIME-HISTORY IN GALS	WCEN	24 95
C	VMAA – MAA. VELOCIII OF HIME-HISIORI IN KINES MVCVCL – MAX NUMPED OF ITEDATION	WGEN	20 26
C	MACICL - MAA, NUMBER OF ILERATION	WGEN	20
C	EKK - KUUI-MEAN-SQUAKE EKKUK FUK UUNVERGENCE IN DECIMAL	WGEN	21
C	FRACTION	WGEN	28
C	UWI(ND) - WORKING AREA	WGEN	29
С	UW2(ND) - WORKING AREA	WGEN	30
С		WGEN	31
С	REMARKS	WGEN	32
С	NN MUST BE EQUAL TO POWER OF 2 NOT LARGER THAN 4096	WGEN	33
С		WGEN	34
С	SUBROUTINES AND FUNCTION SUBPROGRAM REQUIRED	WGEN	35
С	ENVL OHSP VELK FAST CRAC IACC ERES RAND	WGEN	36
С		WGEN	37
	SUBROUTINE WGEN (EM, R, NN, IR, ACC, ND, DT, AMAX, VMAX, MXCYCL, ERR, UW1,	WGEN	38
	* UW2)	WGEN	39
С		WGEN	40
	COMPLEX C(4096)	WGEN	41
	DIMENSION ACC(ND), UW1(ND), UW2(ND)	WGEN	42
	DIMENSION $E(33), X(33), EE(33)$	WGEN	43
	DIMENSION PDIF (2046), PHI (2049), F (2049), T (2049), SV (2049), H(1),	WGEN	44
	* RES (2049, 1), RR (2049)	WGEN	45
	PARAMETER (PI2=6, 283185)	WGEN	46
	DATA $DX/0.03125/.H0/0./.H/0.05/$	WGEN	47
С		WGEN	48
C	PHASE DIFFERENCES	WGEN	49
C		WGEN	-10 50
U	CALL ENVL (EN TR TC TD 22 E 22)	WGEN	51
	DT-TD/DEAL (NN) $(10, 10, 10, 30, 2, 35)$	WCEN	51
	D1 = 1D/REAL(IN) $NN2 = NN/2$	WGEN	52
	NNZ-NN/Z	WGEN	00 E 4
	NFOLD - NNZ + 1	WGEN	54 55
	X(1) = 0.	WGEN	55
	EE(1)=0.	WGEN	56
	D0 110 M=2, 33	WGEN	57
	X(M) = REAL(M-1) *DX	WGEN	58
	EE(M) = EE(M-1) + E(M)	WGEN	59
	110 CONTINUE	WGEN	60
	DO 120 M=2, 33	WGEN	61
	EE(M) = EE(M) / EE(33)	WGEN	62
	120 CONTINUE	WGEN	63
	DO 150 K=1, NN2-2	WGEN	64

		P=RAND (IR)	WGEN	65
		DO 130 J=2,33	WGEN	66
		IF (P. LE. EE (J)) GO TO 140	WGEN	67
	130	CONTINUE	WGEN	68
	140	PDIF(K) = -(X(J-1)+(P-EE(J-1))/(EE(J)-EE(J-1))*DX)*P12	WGEN	69
	150	CONTINUE	WGEN	70
С			WGEN	71
C		PHASE ANGLES	WGEN	72
С			WGEN	73
Ŭ		PHT (2)=0	WGEN	74
		DO = 160 K = 1 NN2 - 2	WGEN	75
		PHI(K+2) = AMOD(PHI(K+1) + PDIF(K) PI2)	WGEN	76
	160	$\begin{array}{c} \text{CONTINIF} \end{array}$	WGEN	77
C	100	CONTINUE	WGEN	70
C		TADCET SDECTDIM AND EIDST FOUDIED ADDDOVIMATION	WGEN	70
C		TARGET SPECIRUM AND FIRST FOURTER AFFROATMATION	WGEN	19
U		$T(1)$ - $TD_{2}Q$	WGEN	00
		$I(I) - ID^{*}Z$.	WGEN	01
		DU = 1/U = K = 2, NFOLD	WGEN	82
	1 50	I(K) = ID/REAL(K-1)	WGEN	83
	170	CONTINUE	WGEN	84
		DO 180 K=2, NFOLD	WGEN	85
		IF (T (K). LE. 2.) GO TO 190	WGEN	86
	180	CONTINUE	WGEN	87
	190	KMIN=K	WGEN	88
		DO 200 K=KMIN, NFOLD	WGEN	89
		IF(T(K).LT.0.02) GO TO 210	WGEN	90
	200	CONTINUE	WGEN	91
		KMAX=NFOLD	WGEN	92
		GO TO 220	WGEN	93
	210	KMAX=K-1	WGEN	94
	220	NE=KMAX-KMIN+1	WGEN	95
		DO 230 K=2, NFOLD	WGEN	96
		CALL OHSP (EM, R, HO, T (K), SVO, K-2)	WGEN	97
		IF(K.LT.KMIN.OR.K.GT.KMAX) SV0=0.	WGEN	98
		F(K) = SVO/TD	WGEN	99
	230	CONTINUE	WGEN	100
		DO 240 K=2, NFOLD	WGEN	101
		CALL OHSP (EM, R, H(1), T(K), SV(K), K-2)	WGEN	102
		IF (K. LT. KMIN. OR. K. GT. KMAX) $SV(K)=0$.	WGEN	103
	240	CONTINUE	WGEN	104
С			WGEN	105
С		ITERATIVE COMPUTATION	WGEN	106
С			WGEN	107
-		ENN=1. /REAL(NN)	WGEN	108
		NCYCL=0	WGEN	109
	250	NCYCL =NCYCL +1	WGEN	110
	200	C(1) = (0, 0, 0)	WGEN	111
		$DO_{260} K=2 NN2$	WGEN	112
		C(K) = F(K) * CMPLX(COS(PHI(K)) SIN(PHI(K)))	WCEN	112
		C(NN+2-K) = CONTC(C(K))	WCEN	11/
	260		WCEN	115
	200	C(NEOLD) = F(NEOLD) * (1 0)	WCEN	110
		$CALL EAST (NN C 4006 \pm 1)$	WCEN	117
		$\mathbf{OLL} \mathbf{IASI} (\mathbf{M}, 0, 4030, 1)$	WGEN	111

			WGEN	118
		DO 270 M=1 NN	WGEN	110
		$\Delta CC(M) = PEAI(C(M))$	WCEN	120
		AUAV = AUAV1 (AUAV ADS (ACC(M)))	WCEN	120
	070	AMAA - AMAA1 (AMAA, ADS (ACC (M)))	WGEN	121
C	270	CONTINUE	WGEN	122
C			WGEN	123
C		BASE LINE CORRECTION	WGEN	124
C			WGEN	125
		CALL CRAC(DT, NN, AMAX, ACC, ND, UW1, UW2)	WGEN	126
		DO 280 M=1, NN	WGEN	127
		C(M) = CMPLX(ACC(M), 0.)	WGEN	128
	280	CONTINUE	WGEN	129
		CALL FAST (NN, C, 4096, -1)	WGEN	130
		DO 290 K=2, NFOLD	WGEN	131
		F(K) = CABS(C(K)) * ENN	WGEN	132
	290	CONTINUE	WGEN	133
С			WGEN	134
С		MODIFICATION OF FOURIER AMPLITUDES	WGEN	135
С			WGEN	136
		CALL ERES (1, H, 1, NFOLD, T, 2049, DT, NN, ACC, ND, 2, VMAX, RES)	WGEN	137
		DO 300 K=2, NFOLD	WGEN	138
		RR(K) = SV(K) / RES(K, 1)	WGEN	139
		F(K) = F(K) * RR(K)	WGEN	140
	300	CONTINUE	WGEN	141
С			WGEN	142
С		ERROR FOR CONVERGENCE	WGEN	143
С			WGEN	144
		EPS=0.	WGEN	145
		DO 310 K=KMIN, KMAX	WGEN	146
		EPS = EPS + (1, -RR(K)) * 2	WGEN	147
	310	CONTINUE	WGEN	148
		EPS=SQRT (EPS/REAL (NE))	WGEN	149
С			WGEN	150
C		IF (FPS LE FRR) GO TO 320	WGEN	151
		IF(NCYCL FO MXCYCL) GO TO 330	WGEN	152
		CO TO 250	WGEN	153
	320	MXCVCI =NCVCI	WGEN	154
	330	FRR=FPS	WGEN	155
	550	DETIEN	WCEN	156
			WCEN	157
			NULN	101

[Example]

Based on the assumption of an earthquake of magnitude 7.3 with an epicentral distance of 25.0 km, calculate the acceleration time history of simulated earthquake motion on the bedrock.

```
С
      DIMENSION ACC(1024), VEL(1024), UW1(1024), UW2(1024), T(513), H(1),
     *
                  RES (513, 1), VRES (513)
      DATA NN/1024/, EM/7. 3/, R/25. 0/, H/0. 05/
      DATA IR/101/, MCYCL/10/, ERR/0.05/
С
      CALL WGEN (EM, R, NN, IR, ACC, 1024, DT, AMAX, VMAX, MCYCL, ERR, UW1, UW2)
      CALL IACC (DT, NN, ACC, VEL, UW1, 1024, VMAX, DMAX)
С
      TD=10.0**(0.31*EM-0.774)
      NFOLD=NN/2+1
      DO 110 K=1, NFOLD
      T(K) = TD/REAL(K)
  110 CONTINUE
      DO 120 K=1, NFOLD
         IF(T(K).LE.2.0) GO TO 130
  120 CONTINUE
  130 KMIN=K
      DO 140 K=KMIN, NFOLD
         IF(T(K).LE.0.02) GO TO 150
  140 CONTINUE
      KMAX=NFOLD
      GO TO 160
  150 KMAX=K-1
  160 NE=KMAX-KMIN+1
      DO 170 K=1, NE
      T(K) = T(K + KMIN - 1)
  170 CONTINUE
      CALL ERES (1, H, 1, NE, T, 513, DT, NN, ACC, 1024, 2, VMAX, RES)
      DO 180 K=1, NE
      VRES (K) = RES (K, 1)
  180 CONTINUE
      STOP
      END
```

Output: The acceleration time history of the simulated earthquake motion is stored in the array *ACC*, the velocity time history integrated from the acceleration time history is stored in the array *VEL*, and the velocity response spectrum with a damping factor of 5% is stored in the array *VRES*. These results can be plotted as shown in Figures (a), (b), and (c). The thin line in Figure (c) is the target Ohsaki's spectrum.

Magnitude M=7.3, Epicentral distance R=25km



Notes: Due to differences in the random number generation program used, the maximum values of acceleration and velocity are slightly different between the English and Japanese versions of the manual.